

PCIM 2014

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> SBE Inc. Booth 9-140 Danfoss Silicon Power Booth 9-360



- Introduction
- Analysis of IGBT input configuration
- Optimized prototype design
 - SBE's overshoot & ring out measurements
 - Testing at Danfoss Silicon Power
- Further work Full scale "power stack" module
- Conclusions
- Questions



- Inverter performance highly dependent of stray inductance value generating voltage overshoot at each turn-off cycle:
 - Snubbers -> added cost and complexity
 - Intelligent gate control -> slow down turn-off transition -> added switching losses
- Ultimate solution is minimizing the total stray inductance -> increased operating voltage and power by 20% - Invested Semiconductor Efficiency

Introduction (2)

- Inductance contributions :
 - DC link capacitor,
 - Bus structure,

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- Internal IGBT branches.
- Different IGBT input configurations will be evaluated
- Inductance and overshoot measurements will be conducted -> validate 20% overshoot reduction with SBE's integrated capacitor/bus



- Flux3D magneto-dynamic finite element analysis platform used to evaluate the inductance of relevant half-bridge IGBT input configurations.
- A laminar bus bar with 0.5mm spacing between copper plates selected as the basis for comparison.
- Harmonic frequency of 10 kHz



- 1. Net impedance unfolded based on the total current flow through conductor cross sections and driving potential,
- 2. Resistive component calculated from total losses in each conductor,

Reactive component impedance established using above calculations - Inductance simulated:

<u>12.8 nH</u> for a "tab style" connection <u>Only 4 nH</u> for a "through hole" connection Analysis of IGBT input (3)





- Comparison of current density distribution for "tab" (a) and "through-hole" (b) inputs.
- Input geometry of a typical 1400A discrete half-bridge module -> defines loop area at input connection.

Optimized prototype design (1)

Optimized single phase capacitor/bus prototype developed through collaboration between SBE & Danfoss Silicon Power



Optimized prototype design (2)

- Capacitors directly integrated to the bus plates -> less copper & better magnetic flux cancellation for low ESL,
- "Ring" form factor also minimizes ESR and thermal resistance of the windings,
- "Through-hole" connections for two half-bridge modules,
- Two auxiliary 300µF capacitors if additional capacitance is required.

SBE's measurements (1)

• Overshoot testing setup:

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- Integrated sensing resistor for accurate measurement of turn-off current,
- Overshoot voltage measured at the IGBT terminals will determine inductance contribution of the capacitor and bus,
- SBE's "ring out" test method correlates with overshoot testing -> Validated by measuring customized & standard parts – results also correlate with customer testing and simulations.



SBE overshoot testing apparatus – used also to validate "ring out" test ^[*] measurements

[*] E. D. Sawyer, "Low Inductance - Low Temp Rise DC Bus Capacitor Properties Enabling the Optimization of High Power Inverters", Proceedings of PCIM, Nuremberg, Germany, May 2010



Measured inductances for the optimized capacitor and bus structure using "ring out" test method.

Testing at Danfoss Silicon Power (1)

Comparison:

SBE optimized capacitor and bus bar structure

VS

Bus bar from Danfoss power stack equipped with an already low stray inductance film can style capacitor bank

Double pulse test applied to measure overvoltage during turn-off and di/dt and ΔV during turn-on to calculate the stray inductance for both cases.

Testing at Danfoss Silicon Power (2)



Bus bar with capacitors: left: Danfoss, right SBE Power Ring Capacitors



Schematic of the test setup and probe placement

Testing at Danfoss Silicon Power (4)

- Measurements taken at lower transistor while upper IGBT is kept in the off condition,
- Base plate temperature of module under test maintained at 25C,
- Differential voltage probes connected between terminals 1-2 & terminals 3-2,
- Rogowski Current Transducers placed around module terminals 10 & 12.

Testing at Danfoss Silicon Power (5)

Total stray inductance calculated by measuring di/dt and the DC-link voltage dip at the AUX terminals at IGBT module at turn on: $L_s = \Delta V x di/dt$

Standard capacitor bus bar	SBE optimized module bus bar	
DC-link voltage: 1100V		
Peak current during turn on: 1200A		
ΔU = 296 V	ΔU = 224 V	
dI/dt = 12.3 kA/µS	dI/dt = 14.7 kA/µS	
L _s = 24 nH	L _s = 15 nH	

Testing at Danfoss Silicon Power (6)

Partial stray inductance calculated by measuring di/dt and the voltage V_{ce} across the whole module, does not take into account the IGBTs internal inductance

SBE optimized module bus bar		
ΔU = 65 V dI/dt = 14.7 kA/μS		
Stray inductance of capacitors & bus bar only	Stray inductance of IGBT modules only	
L _s = 4.4 nH	L _{IGBTs} ~ 10 nH	

Results compatible with datasheet claims



Voltage measurements at turn off, show **20% less overshoot** when using SBE Power Ring optimized DC Link bus bar

Standard capacitor bus bar	SBE optimized module bus bar	
DC-link voltage: 1100V		
ΔU = 448 V	ΔU = 348 V	
Peak current during turn off =	Peak current during turn off =	
1000 A	1046 A	
20% less overshoot using SBE Power Ring technology		

Testing at Danfoss Silicon Power (8)



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Example of SBE module turn off oscilloscopic measurement:

Purple curve = total current

Blue curve = voltage at IGBT terminals

Conclusions (1)

Optimized DC link capacitor/bus configuration with ESL < 5nH (magneto-dynamic analysis, ring-out & overshoot measurement validation) Reduction in overshoot voltage of more than 20% 20% increase in inverter power achieved with the same investment in silicon Advantage in the highly competitive alternative energy market space.





Thank you